Joint Institute for Nuclear Research Frank Laboratory of Neutron Physics



OPTIMIZATION OF NEUTRON PHYSICS PARAMETERS OF THE NEW PULSED NUCLEAR REACTOR NEPTUNE

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GOALS AND OBJECTIVES

• The NEPTUNE reactor is one of the proposed alternatives to replace the current IBR-2M reactor after it is out of service.

• It is supposed to work as a neutron source within the Laboratory of Neutron physics at the Joint Institute for Nuclear Research in the city of Dubna.

• A technical goal was set, to obtain an average neutron flux higher than that from the current IBR-2M reactor by one order of magnitude.

1- MAIN FEATURES OF THE REACTOR NEPTUN:

- 1. The proposed source will have a peak neutron flux up to $5 \times 10^{17} n/sec^1 cm^2$ and a time average flux density of up to $1.2 \times 10^{14} n/sec^1 cm^2$ (in IBR 2M: 0.7×10^{16} and 10^{13}).
- 2. Using the fission-threshold isotope Np-237 for the first time as a nuclear fuel, resulting $\frac{1}{5}$ in:

- The generation time of fast neutrons (τ) in the neptunium core is 5-7 times shorter than that in the core with plutonium (the task of having a short pulses of neutrons becomes easier).

- A low value of the effective delayed neutrons fraction (β -eff) determines a low background power in the intervals between pulses (3-4 times less Pu).

- Possibility of using neutron moderating materials as a Reactivity Modulator (RM) or control rod (like hydride's metal TiH_{2} , YH_{2}).

- There is no reactivity effect from the fuel burnup (it is possible to work without additional fuel loading during the entire reactor cycle):

Np-237 (n absorption) → Np-238 (β-decay, (2.117 days) → Pu-238 (Fissionable material)



2-THE MAIN PARAMETERS OF THE REACTOR:

| Parameter | Value | | | |
|---|--------------------------|--|--|--|
| AVERAGE THERMAL POWER , MW | 12 - 15 | | | |
| OPERATING MODE | pulsed | | | |
| PULSE FREQUENCY, Hz | 10 | | | |
| FUEL | NpN | | | |
| CLADDING MATERIAL OF FUEL RODS | S.Steel | | | |
| COOLER | Na | | | |
| REFLECTOR | NICKEL ALLOY + BERYLLIUM | | | |
| MODERATOR, PREMODERATOR | water, beryllium | | | |
| COOLANT TEMPERATURE AT THE INLET TO THE CORE AND AT THE OUTLET, ⁰ C | 290-390 | | | |
| PRESSURE DROP THROUGH THE CORE, Pa | 0,33×10 ⁵ | | | |
| FLUENCE ON THE REACTOR SURROUNDING'S FOR 20,000 h, n / CM ² | 4,1·10 ²² | | | |
| AVERAGE NEUTRON THERMAL FLUX AT THE SURFACE OF WATER MODERATOR, 2π- equivalent 10 ¹³ cm ⁻² ·sec ⁻¹ | 12 | | | |
| EFFECTIVE FRACTION OF DELAYED NEUTRONS | 0,00131 | | | |
| GENERATION TIME OF THE SPONTANEOUS NEUTRONS, n.sec | 8 | | | |



Reactor core and reactivity modulator



Vacuum sector

4- REACTOR CONTROL SYSTEM:

- Reactor control system consists of 3 groups:
 - 1- automatic control system;
 - 2- burnup balancer system;
 - 3- emergency shutdown system.
- The first and second systems are located around the reactor core and act as a neutron reflector (Ni blocks).
- The third system is located inside the reactor core and consists of blocks that are either neutron moderators (TiH_2 or YH_2) or neutron absorbers (B_4C).
- According to the regulations governing the operation of research reactors stipulate that: the control system must provide a subcriticality of 2% (Keff=0.98) in the temporary shutdown mode.

| | Worth (effect) of C. B. % | | | | |
|-------------------------|------------------------------|------------------|--|--|--|
| Control block (C.B.) | Material of inside core C.B. | | | | |
| | YH ₂ | B ₄ C | | | |
| 1 (1+2) | 0.94 (2.0) | 0.75(1.6) | | | |
| 1+ <mark>2</mark> +3+4 | 4.0 | 3.2 | | | |
| 5 | 0.53 | 0.54 | | | |
| 5+6 | 1.04 | 1.1 | | | |





- Technical problem:
- The temperature of TiH2 near the empty sector reaches **560** degrees.
- It is known that the use of TiH2 is limited to a temperature of **400** degrees. After that, the hydrogen content in TiH2 decreases and the effectivity of RM decreases.
- Technical solution:
- It is suggested to install additional nickel reflectors on the border of the empty sector and sectors containing TiH2.
- Both the width of the vacuum sector (30,35,40,45 cm) and the width of the of added Ni plate (0,5,10) have been changed, and the energy absorbed in TiH2 was calculated for each variant.



Temperature distribution in TiH2 near the vacuum sector.



Addition Ni reflectors between the vacuum sector and TiH2 sectors

- The obtained results:



Dependence of the maximum absorbed heat in TiH2 (W/cm3), on changes in the vacuum width and Ni thickness

| | | Max | ximum absorbed | heat in Til | H2, W/ | /cm3 | |
|---------------------|---------|---------|----------------|-------------|--------|----------|---------|
| | 0 cm | n Ni | 5 cm | n Ni | | 10 cm Ni | |
| | Right | left | Right | left | | Right | left |
| 30 cm vacuum | 9,65634 | 10,5207 | 6,66692 | 7,75357 | | 4,48174 | 5,43119 |
| 35 cm vacuum | 8,5089 | 9,52174 | 5,55672 | 6,59312 | | 3,82486 | 4,4615 |
| 40 cm vacuum | 7,41187 | 8,45502 | 4,71953 | 5,61119 | | 3,22433 | 3,61275 |
| 45 cm vacuum | 6,3444 | 7,32191 | 4,00864 | 4,68787 | | 2,59712 | 2,93969 |









Absorbed heat in TiH2 with installing 10 cm Ni reflector, W·cm-3 TiH2 gearbox-supps Drive shaft Electric motor

Gearbox



- The obtained results:



Temperature distribution in TiH2 without installing an additional Ni reflector, W·cm-3



Temperature distribution in TiH2 with installing 10 cm Ni reflector, W·cm-3



- The obtained results:



1,016 -1,014 -Эффективный коэффициент 1,012 0,998

Reactivity course for options: vacuum window width 40 cm



- The obtained results:



Dependence of the maximum modulator effect (%) and α - parameter (cm-2) on changes in the vacuum width and Ni thickness

| | 30 cm | 30 cm | 30 cm | 35 cm | 35 cm | 35 cm | 40 cm | 40 cm | 40 cm | 45 cm | 45 cm | 45 cm |
|------------------------------------|----------|----------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| | vacuum, | vacuum, | vacuum, | vacuum | vacuum, |
| | 0 см Ni | 5 см Ni | 10 см Ni | 0 см Ni | 5 см Ni | 10 см Ni | 0 см Ni | 5 см Ni | 10 см Ni | 0 см Ni | 5 см Ni | 10 см Ni |
| Maximum modulator effect , % | 6,29% | 7,13% | 7,50% | 6,73% | 7,37% | 7,59% | 7,01% | 7,46% | 7,61% | 7,17% | 7,48% | 7,59% |
| 🛛 -parameter, cm-2 | 1,37E-04 | 1,24E-04 | 9,82E-05 | 1,21E-04 | 9,88E-05 | 6,81E-05 | 9,01E-05 | 6,04E-05 | 3,85E-05 | 5,40E-05 | 2,92E-05 | 1,28E-05 |



Thanks for attention. Any questions??





Neutron sources

<u>B) Denes sources</u>: 2- Periodic Pulsed power reactors:

| | IBR-1 1960 - 1968 | IBR-30 19 | IBR-2 с 1984 г | IBR-3 (NEPTUNE) |
|---|----------------------|----------------------|---|-------------------------|
| Thermal power | 1- 3 к Wт | 20 кWт | 2 MWт | 12-15 MWт |
| Fissile material | Pu-239 metal | Pu-239 metal | PuO2 | Np-237, NpN |
| Reactivity modulator, frequency | U-235 5-50 Hz | U-235 0.1 - 10 Hz | Moveable reflector from Ni 5-25 Hz | TiH2+and void, 10 Hz |
| The half width pulse | 40 μs | 70 µs | 240 μs | ~260-µs |
| Neutron flux at the surface of moderators, cM ² / s, | ~10 ¹⁰ | 10 ¹¹ | 10 ¹³ | 10 ¹⁴ |

Neutron sources

B) Denes sources : 2- Periodic Pulsed power reactors:

- In 1955- in the Obninsk Pysical-Power institute (Russia), D.I. Blokhintsev suggested the idea of a periodic pulsed reactors with mechanically periodically reactivity modulation.
- To combines the best features of Aperiodic reactors (pulsed nature without any choppers time of flight) and steady state power reactors (good enough fluence to neutron spectroscopy).



Dmitry Blokhintsev (1907-1979)



The course of reactivity and power of the reactor during the development of the power pulse

4- REACTOR CONTROL SYSTEM:

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 $\varepsilon(t)$

W(t)

 $\varepsilon(t)$

 $\mathbf{W}_{\mathbf{m}}$

W(t)